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### **Master Thesis**

# Structural Optimisation of Midship Region for Ro-Pax Vessel in Early Design Stage using FEA

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# Optimisation

- the process of decision making when a number of alternative choices are available
- an optimal solution has to be determined with regard to specific criteria
- taking into account the restrictions and constraints set by the environment
- Ship design a typical optimisation problem involving multiple and frequently contradictory objective functions and constraints

- Ships need to be optimised for
  - cost effectiveness
  - highest operational efficiency or lowest required freight rate
  - passenger and crew comfort and safety
  - minimum environmental impact, etc.
- Optimisation often requires minimization or maximization of property(ies) of the structure under given load cases and constraints

- Development of an integrated platform for the optimisation of midship region of Ro-Pax vessel using ANSYS<sup>®</sup> APDL, as finite element tool and modeFRONTIER<sup>®</sup>, as optimisation tool
- No manual intervention in the GUI of the integrated platform
- Determination of optimum scantlings and thereby the minimum weight (objective) of the midship region of Ro-Pax vessel
- Developing polynomial response surfaces (RSM) to replace the FEM package to reduce calculation time

### 3. Methodology



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### Stiffened Panels

- basic building blocks in ships and marine structures
- also find applications in box girder bridges, nuclear power plants, etc.
- reduction in stiffened panel weight without losing their structural integrity yields reduction in ship's weight
- optimisation process to test the codes developed in ANSYS<sup>®</sup> APDL and understand the working of ANSYS<sup>®</sup> and modeFRONTIER<sup>®</sup> coupled loop

### - Seven design variables

- plate thickness
- number of longitudinal stiffeners
- number of transverse stiffeners
- longitudinal stiffener web height and web thickness
- transverse stiffener web height and web thickness
- Weight Objective function

- Optimisation loop using ANSYS<sup>®</sup> APDL



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- Convergence history for **Objective** function (**Weight** of the stiffened panel)



## Response Surface Method (RSM)

- Response surface using second order polynomial regression model

$$\begin{split} & \mathsf{W} = 836.09904 + 233.42986^*\mathsf{Y}_1 + 168.72417^*\mathsf{Y}_2 + 116.81434^*\mathsf{Y}_3 + \\ & 155.13404^*\mathsf{Y}_4 + 114.26292^*\mathsf{Y}_5 + 190.34547^*\mathsf{Y}_6 + 136.51625^*\mathsf{Y}_7 - \\ & 19.93504^*\mathsf{Y}_1^*\mathsf{Y}_2 + 12.16043^*\mathsf{Y}_1^*\mathsf{Y}_3 - 32.46640^*\mathsf{Y}_1^*\mathsf{Y}_4 + 16.12237^*\mathsf{Y}_1^*\mathsf{Y}_5 + \\ & 5.33439^*\mathsf{Y}_1^*\mathsf{Y}_6 - 13.15543^*\mathsf{Y}_2^*\mathsf{Y}_3 + 114.30040^*\mathsf{Y}_2^*\mathsf{Y}_4 + 90.76182^*\mathsf{Y}_2^*\mathsf{Y}_6 - \\ & 10.15464^*\mathsf{Y}_2^*\mathsf{Y}_7 + 76.85179^*\mathsf{Y}_3^*\mathsf{Y}_5 - 16.71419^*\mathsf{Y}_3^*\mathsf{Y}_6 + 41.21212^*\mathsf{Y}_3^*\mathsf{Y}_7 - \\ & 54.10183^*\mathsf{Y}4^*\mathsf{Y}_5 + 70.96034^*\mathsf{Y}_4^*\mathsf{Y}_6 + 19.71127^*\mathsf{Y}_4^*\mathsf{Y}_7 + 58.45976^*\mathsf{Y}_5^*\mathsf{Y}_7 - \\ & 11.18839^*\mathsf{Y}_2^2 + 21.54268^*\mathsf{Y}_4^2 + 3.36939^*\mathsf{Y}_7^2 \end{split}$$

- **Relative difference in the weight** between FEM and RSM is less than **4%**
- Time taken for one calculation in a machine with Intel<sup>®</sup> Core i3, 2.0 GHz CPU and 4GB RAM
  - FEM 30 seconds
  - RSM milliseconds

### Ro-Pax Vessels

- designed to transport vehicles and passengers efficiently
- midship structural design can be considered as a basic structural problem
- the major part of hull follows the pattern of midship section
- provides an approximate estimation of hull weight

Length overall	220.00 m
Length between perpendiculars	210.00 m
Breadth	30.00 m
Depth	9.0 m
Draft	6.50 m
Block coefficient	0.629
Displacement	28000.00 t

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5. Midship Region Optimisation of Ro-Pax Vessel



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Load cases based on BV Rules

Load Conditions	Description
1	Full load on decks + (a+) + Sagging
2	Full load on decks + (a+) + Hogging
3	Full load on decks + (a-) + Sagging
4	Full load on decks + (a-) + Hogging
5	Full load on decks + (b) + Sagging
6	Full load on decks + (b) + Hogging
7	Full load on decks + (c+) + Sagging
8	Full load on decks + (c+) + Hogging
9	Full load on decks + (d+) + Sagging
10	Full load on decks + (d+) + Hogging
11	Ballast Condition + (a+) + Hogging

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- Finite element model of midship region selected between two main frames,
  4.8m extension.
- SHELL181 elements for plates
- BEAM188 elements for stiffeners
- Load case 2 considered
- RIGID elements are employed on ends of the model
- 2 Materials are available (Mild Steel and HSS)

Material	Young's modulus	Yield Strength
	(MPa)	(MPa)
Mild Steel	206000	235
High Strength Steel	206000	355



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# Midship Region Optimisation

- 58 Design variables in total
  - 30 for representing plate thicknesses
  - 10 for stiffener geometry
  - 18 for stiffener spacing
- Constraints imposed

 $\begin{cases} 6 \ mm \le t_p \le 17 \ mm \\ 400 \ mm \le S_s \le 700 \ mm \end{cases}$ 

- Stiffener geometry database available from shipyard
- Allowable stress values for the materials are calculated using the below equation (BV Rules NR467, Part B, Chapter 7, Section 3)

$$\sigma_{VM} = \frac{R_y}{\gamma_R \gamma_M}$$

- Resistance partial safety factor,  $\gamma_R = 1.2$
- Material partial safety factor,  $\gamma_M = 1.02$

- Midship structural optimisation loop



 Convergence history for Objective function (Weight of the midship region of Ro-Pax vessel)



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## **Comparison of Results with RSM**

$$\begin{split} & \mathsf{W} = 365.9242 + 4.3065^*\mathsf{Y}_1 + 8.4978^*\mathsf{Y}_3 + 18.1669^*\mathsf{Y}_5 + 2.3236^*\mathsf{Y}_6 + 21.1239^*\mathsf{Y}_8 + \\ & 3.3606^*\mathsf{Y}_{10} + 7.6034^*\mathsf{Y}_{11} - 2.3262^*\mathsf{Y}_{12} + 9.8896^*\mathsf{Y}_{13} + 3.5447^*\mathsf{Y}_{14} - 2.2277^*\mathsf{Y}_{15} + \\ & 3.8099^*\mathsf{Y}_{18} + 8.3646^*\mathsf{Y}_{19} + 4.6476^*\mathsf{Y}_{20} + 4.1471^*\mathsf{Y}_{23} - 4.007^*\mathsf{Y}_{24} + 24.7047^*\mathsf{Y}_{25} + \\ & 8.0861^*\mathsf{Y}_{26} - 2.3731^*\mathsf{Y}_{28} + 9.2455^*\mathsf{Y}_{31} + 1.9007^*\mathsf{Y}_{32} + 2.4002^*\mathsf{Y}_{33} + 16.3632^*\mathsf{Y}_{34} + \\ & 5.0619^*\mathsf{Y}_{35} + 7.6309^*\mathsf{Y}_{37} + 17.3196^*\mathsf{Y}_{38} + 10.2807^*\mathsf{Y}_{39} + 31.5779^*\mathsf{Y}_{40} - 29.7439^*\mathsf{Y}_{41} \end{split}$$



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- Optimisation convergence history shows the ability to couple ANSYS<sup>®</sup> and modeFRONTIER<sup>®</sup> for structural optimisation.
- Feasibility of an automated structural optimisation loop achieved.
- Significant reduction of structural weight is possible through the optimisation in early design stage.
- Parametric code developed using ANSYS<sup>®</sup> APDL can be applied to different kind of ships with slight modifications.
- Response surface method is a reliable tool to replace the existing optimisation loops to reduce the calculation time.

- Frame spacing can be considered as design variable
- A coupled tool between CAD, FEA and optimisation software
- Loads from CFD analyses instead of rule based loads
- Load case 2 considered. All identified load cases have to be included.

